

# Pyroelectric and Dielectric Properties of Ferroelectric Films With Interposed Dielectric Buffer Layers

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## Abstract

We theoretically investigate dielectric and pyroelectric properties of ferroelectric films with linear dielectric buffer layers. Computations were carried out for multilayers consisting of  $\text{PbZr}_{0.2}\text{Ti}_{0.8}\text{O}_3$  with  $\text{Al}_2\text{O}_3$ ,  $\text{SiO}_2$ ,  $\text{Si}_3\text{N}_4$ ,  $\text{HfO}_2$  and  $\text{TiO}_2$  buffers on metalized Si. We show that the dielectric and pyroelectric properties of such multilayers are not significantly diminished by the presence of the buffer layer compared to their homogeneous ferroelectric counterparts. Indeed, stacked multilayer ferroelectric films with dielectric buffers can be used to not only provide high electric field breakdown strength films, but may be designed to optimize pyroelectric and dielectric properties of ferroelectric multilayer films.

**Keywords:** pyroelectric, electrocaloric, ferroelectrics, multilayers

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The origin of the dielectric (DE) and pyroelectric properties of ferroelectric (FE) materials and their thin film embodiments have been well understood for several decades. Moreover, their dependencies upon: crystal structure, temperature, applied electric field and stress, thickness, etc., have been studied extensively both experimentally and theoretically.<sup>1-7</sup> Most recently, however, the behavior of this class of thin film materials at very high fields,  $\geq 100$  MV/m, has become of interest for their enhanced electrocaloric response.<sup>8</sup>

Non-polymeric bulk FE materials cannot easily sustain electric fields exceeding  $\sim 1$  MV/m due to the density and hence aggregated number of defects within the materials.<sup>8,9</sup> Thin film FEs, however, when deposited upon suitable substrates have been shown to support electric fields of much greater magnitude due to their improved crystallinity, smaller number of crystalline and electronic defects, and high densities within the associated volume element comprising the film.<sup>10-12</sup> Mechanisms of high field failure and current leakage fall into one of the two following categories: bulk-limited and interface-limited conduction. Of all the possible leakage mechanisms, the three most commonly observed in FE perovskite oxides are interface-limited Schottky emission, bulk-limited space-charge-limited conduction and bulk-limited Poole-Frenkel emission.<sup>13,14</sup> Thus, even thin film FE often cannot easily sustain repeated high electric field cycling.

It has been, however, shown experimentally that adding a DE buffer layer will improve leakage and loss characteristics of ferroelectric devices under high field.<sup>15-18</sup> For example,  $\text{Ba}_x\text{Sr}_{1-x}\text{TiO}_3$  (BST) films grown on sapphire with a 9 nm  $\text{SrTiO}_3$  (STO) buffer layer has a lower leakage current ( $\sim 1 \times 10^{-8}$  A/cm<sup>2</sup> at 0 V) compared to a BST monolayer with no buffer layer ( $\sim 1 \times 10^{-7}$  A/cm<sup>2</sup> at 0 V)<sup>19</sup>; and, therefore, motivate adoption of solutions taken from the integrated circuit (IC) and MEMS device community to address such problems. Indeed, it has

long been known that interposing a high quality DE (e.g.,  $\text{Si}_3\text{N}_4$ , or similar) between an inferior material of lesser electric field breakdown strength can substantially improve the overall field strength of a multilayer.<sup>20</sup> However, it is a matter of rudimentary physics that the DE properties of such a multilayer will often be dependent upon the material with the smaller relative permittivity – subject to geometrical film thickness considerations. It is this latter proviso that we explore theoretically in this paper; namely the role of an interposed thin film DE on the pyroelectric and DE properties of the multilayer. To do this, we use a non-linear thermodynamic model and investigate the room temperature ( $\text{RT}=25^\circ\text{C}$ ) DE and pyroelectric properties of FE/DE bilayers. It is known that FE multilayers or compositionally graded structures exhibit unusual properties that have been attributed to elastic and electro-mechanical interactions.<sup>21–23</sup> A thermodynamic analysis carried out for STO/BaTiO<sub>3</sub> (BTO) bilayers has revealed the presence of a critical relative thickness of STO at which a large DE response is expected.<sup>21</sup> This anomaly is explained through the presence of internal (depolarizing) fields that suppress ferroelectricity at a critical volume fraction of STO. In this study we use a similar methodology to investigate the pyroelectric properties of  $\text{Pb}(\text{Zr}_{0.2}\text{Ti}_{0.8})\text{O}_3$  PZT(20/80) as a prototypical FE and several distinct materials for the DE buffer layers including alumina ( $\text{Al}_2\text{O}_3$ ), silica ( $\text{SiO}_2$ ), silicon nitride ( $\text{Si}_3\text{N}_4$ ), hafnia ( $\text{HfO}_2$ ), and titania ( $\text{TiO}_2$ ). We show here that the pyroelectric response is marginally affected by the presence of buffer layers below a critical thickness. Lastly, we find that “designed” multilayer FE films with buffer layers tailored to critical thicknesses can be used to optimize properties of FE films.

Consider a (001)-textured, mono-domain PZT 20/80 film on a Si substrate with linear DE buffer layers schematically shown in Fig. 1(a) with the linear DE being  $\text{Al}_2\text{O}_3$  as an example. We

assume that the films are deposited at a growth temperature ( $T_G$ ) of 550°C and then cooled to RT. The non-equilibrium excess free energy of such a system in the FE state can be expressed as:

$$\mathbf{G} = (1 - \alpha) \cdot \mathbf{G}_1(P_1, T, u_T, E) + \alpha \cdot \mathbf{G}_2(P_2, E) + \frac{1}{2} \alpha (1 - \alpha) \frac{1}{\epsilon_0} (P_1 - P_2)^2 + \frac{G_S}{h} \quad (1)$$

where  $\alpha$  is the layer fraction of the buffer layer (defined as the thickness of the buffer layer divided by the total film thickness),  $u_T$  is the in-plane thermal strain due to thermal expansion mismatch between PZT and Si ( $\Delta\alpha = \alpha_{PZT} - \alpha_{Si}$ ) and given by  $u_T = \int_T^{T_G} \Delta\alpha dT$ . The third term in Eq. (1) is the contribution due to interlayer coupling.  $G_i$  are the uncoupled free energies of each layer and given by:

$$G_1(P_1, T, u_T, E) = G_{0,1} + \tilde{a}_1 P_1^2 + \tilde{b}_1 P_1^4 + c_1 P_1^6 + \frac{u_T^2}{S_{11} + S_{12}} - EP_1 \quad (2)$$

$$G_2(P_2, E) = \frac{P_2^2}{2\epsilon_0 \epsilon_{R,2}} - EP_2 + G_{EL} \quad (3)$$

where  $\tilde{a}_i$ ,  $\tilde{b}_i$ , and  $c_i$  are the DE stiffness coefficients of the FE and  $S_{ij}$  are the elastic compliances at constant polarization, for which values were obtained from the literature.<sup>24-27</sup> The modified coefficients  $\tilde{a}_i$  and  $\tilde{b}_i$  in Eq. (2) read;

$$\tilde{a}_1 = a_1 - \frac{2Q_{12}}{S_{11} + S_{12}} u_T \quad \text{and} \quad \tilde{b}_1 = b_1 + \frac{Q_{12}^2}{S_{11} + S_{12}} \quad (4)$$

where  $Q_{ij}$  are the cubic electrostrictive coefficients of PZT.  $\epsilon_0$  is the permittivity of vacuum and  $\epsilon_{R,2}$  is the DE constant of the buffer layer (layer 2). We note that layer 2 is a linear DE and the elastic energy  $G_{EL}$  in Eq. (3) is not polarization dependent. The equilibrium polarizations  $P_1^0$  and  $P_2^0$  are obtained from Eqs. (2), (3) and from the equations of state  $\partial G / \partial P_1 = 0$  and  $\partial G / \partial P_2 = 0$ .

Pyroelectric and DE properties are then computed from the relevant Maxwell's relations such that:

$$p = \frac{dP_S}{dT} + \int_0^E \left( \frac{\partial \varepsilon}{\partial T} \right)_E dE \quad (5)$$

$$\langle \varepsilon_R \rangle = \frac{1}{\varepsilon_0} \frac{d\langle P \rangle}{dE} = \frac{1}{\varepsilon_0} \left[ (1-\alpha) \frac{dP_1^0}{dE} + \varepsilon \frac{dP_2^0}{dE} \right] \quad (6)$$

where  $\langle P \rangle = (1-\alpha)P_1^0 + \alpha P_2^0$  is the average polarization. The second term in Eq. (5) is the DE contribution to the total pyroelectric response and it can be neglected for films in the polar FE state in the absence of external bias.<sup>26</sup>

Fig. 1(b) shows the average out of plane polarization of PZT 20/80 films for  $T_G=550^\circ\text{C}$  as a function of  $\text{Al}_2\text{O}_3$  layer fraction on platinum coated Si. The net polarization decreases rapidly with increasing thickness  $\text{Al}_2\text{O}_3$  (with a zero spontaneous polarization,  $P_S$ ) due to large polarization mismatch between the FE and DE layer. Specifically, at a critical thickness of only ~2% of the PZT;  $P_S$  is zero in the absence of a bias field. Application of an electric field to compensate for the polarization decay shifts the critical thickness to a larger value. Conversely, the average dielectric permittivity ( $\varepsilon_R$ ) and pyroelectric,  $p$ , response of the composite structure gradually increases with increasing  $\text{Al}_2\text{O}_3$  layer fraction as can be seen in Figs. 1(c) and 1(d). This seemingly counterintuitive result is related to two factors: electrostatic coupling between layers and a shift in the Curie temperature to lower temperatures as a result of the interfacial strain between the FE and the interposed DE layer. In this example, an abrupt change of spontaneous polarization at the critical buffer layer fraction increases  $\varepsilon_R$  for bulk PZT from 85 to 310 for structures with 1.00%  $\text{Al}_2\text{O}_3$  interposed between a platinum coated films clamped on Si substrate with a growth temperature  $T_G=550^\circ\text{C}$ . Fig. 1(d) plots the pyroelectric coefficient of

PZT-Al<sub>2</sub>O<sub>3</sub> bilayers as a function of the buffer layer fraction. Adding a DE layer to PZT films drastically improves the pyroelectric properties. In this same example, a bilayer composed a PZT film with 1.00% Al<sub>2</sub>O<sub>3</sub> shows a pyroelectric coefficient of 0.070  $\mu\text{C}/\text{cm}^2\text{ }^\circ\text{C}$  which is 80% higher than the value computed for PZT 20/80 monolayer on Si. Remarkably, these results run counter to approximations that describe DE bi-layers as capacitors in series.<sup>28,29</sup> Calculations for Si<sub>3</sub>N<sub>4</sub> as the buffer layer yield similar results. For PZT with  $T_G=550^\circ\text{C}$ , the critical fraction of Si<sub>3</sub>N<sub>4</sub> is 1.75%. This is because the bulk dielectric permittivity of Si<sub>3</sub>N<sub>4</sub> and Al<sub>2</sub>O<sub>3</sub> are similar (7 and 8, respectively). For a bilayer with Si<sub>3</sub>N<sub>4</sub> fraction equal to 1.00%, the  $\epsilon_R$  and the pyroelectric coefficients are  $\sim 360$  and 0.078  $\mu\text{C}/\text{cm}^2\text{ }^\circ\text{C}$ . The above findings are consistent with the fact that active electrocaloric and pyroelectric thin film devices often have active FE layer thicknesses of  $\sim 1000$  nm, whereas the thicknesses necessary to achieve high DE field breakdown strengths in interposed DE layers are often on the order of 1-10 nm, making these results encouraging for the next generation pyroelectric and electrocaloric devices.

Fig. 2 shows the relationship between DE and pyroelectric properties as a function of the buffer layer fraction for four different DEs. The configuration of bilayers with SiO<sub>2</sub>, HfO<sub>2</sub> and TiO<sub>2</sub> is identical to the one shown in Fig. 1 (a). It is seen, that due to the polarization mismatch between the layers, a critical layer fraction exists at which both the pyroelectric coefficient and  $\epsilon_R$  rapidly increase. For alumina, this critical fraction is about 1.95%. For SiO<sub>2</sub>, Si<sub>3</sub>N<sub>4</sub>, HfO<sub>2</sub> and TiO<sub>2</sub> these layer fractions are approximately 1.10%, 1.75% 5.00%, and 20.40%, respectively. There is a direct relationship between the critical layer fraction and the DE constant, namely that materials with higher intrinsic permittivity more closely couple to the polarization, much as we might expect from our simple capacitor models in the absence of induced FE to DE phase transitions.

Fig. 3 plots the critical layer fraction as a function of relative DE permittivity of the DE buffer layer for titanium rich PZT compositions (which progressively shift the Curie temperature). Bulk DE permittivities for common DE materials are denoted on the top axis. The critical layer fraction increases with increasing bulk DE constant of the buffer layer. The DE constants of common DEs are marked on the top axis of Fig. 3. It is also noted that for PZT compositions with larger zirconium concentrations the critical layer fraction increases at a faster rate. For example, the critical layer fraction for a buffer layer with DE constant of 40 on PZT 0/100 ( $\text{PbTiO}_3$ ) is 9.00% compared to PZT 40/60 for which it is about 4.50%. Consequently, control of thickness during deposition/growth and the choice of the buffer layer can be exploited to optimize the pyroelectric coefficient as well as the DE constant of the FE multilayer.

It should be noted that these calculations are carried out for monodomain films that are assumed to be perfectly (001)-aligned. PZT films grown on platinized Si substrates are predominantly (111) textured.<sup>30</sup> Therefore the polarization and pyroelectric vector components lie along [111] and hence the computed values are lowered for such films.<sup>26,31</sup> It is therefore necessary to find synthesis routes that will produce (001)-textured films to maximize the pyroelectric response of the films and having a buffer layer may help. Moreover, the interfacial energy due to polarization gradients at the interlayer interface is neglected in Eq. (1) when computing the equilibrium properties of the bilayers. This is a valid assumption provided that the individual layers that make up the multilayer are sufficiently thick. As seen in Fig. 3, the critical layer fraction is  $\sim 2.5\%$  for a DE with  $\epsilon_r=10$ . For a 100 nm-thick bilayer, the required thickness of the DE should therefore be  $\sim 2.5$  nm for which the polarization distribution at the layer interface may have a substantial effect on the DE and pyroelectric properties.

To facilitate better thermal transport through a pyroelectric device, the substrates are back-etched to remove Si which is not a good thermal conductor.<sup>32</sup> This reduces the time coefficient of the detector and increases the figure of merit.<sup>33,34</sup> We have carried out computations for such a case where Si is assumed to be removed from the bilayer prior to growth/deposition. For a PZT 20/80 with an Al<sub>2</sub>O<sub>3</sub> buffer layer with  $\alpha=1.00\%$  at  $T_G=550^\circ\text{C}$ , the DE constant and the pyroelectric coefficient ( $\sim 145$  and  $0.054 \mu\text{C}/\text{cm}^2 \text{ }^\circ\text{C}$ ) are actually lower than for bilayers on Si. This is related to the fact that thermal strains in PZT 20/80 may actually improve DE and electrothermal properties as shown in Kesim *et al.*<sup>35</sup> and Zhang *et al.*<sup>25</sup> by shifting the Curie temperature to RT.

Prior studies by the IC and MEMS community have shown that the DE strength of DE films may be increased nearly tenfold by interposing high breakdown strength DEs of 1-10 nm thickness.<sup>20</sup> Such works, together with the findings of this paper suggest that the performance of pyroelectric based energy conversion devices (thermal to electric and electric to thermal) could benefit from this approach. Specifically, it has been demonstrated that the field dependence of the temperature lifts attainable through the electrocaloric effect are power law of coefficient greater than 1. Hence, application and sustainment of fields  $>100\text{MV}/\text{m}$  significantly improve the temperature lifts produced from the materials now widely being studied in this active field of research.



## FIGURE CAPTIONS

- Figure 1:** (Color online) (a) Schematic of PZT 20/80 film with Al<sub>2</sub>O<sub>3</sub> buffer layer on Si. Room temperature (b) polarization, (c) small signal relative dielectric permittivity, and (d) pyroelectric coefficient curves of PZT 20/80 as a function of Al<sub>2</sub>O<sub>3</sub> layer fraction for  $T_G=550^\circ\text{C}$  on Si for  $E=0, 50, 100, 150,$  and  $200$  kV/cm.
- Figure 2:** (Color online) Pyroelectric coefficient and relative dielectric permittivity of PZT 20/80 as a function of (a) Al<sub>2</sub>O<sub>3</sub>, (b) SiO<sub>2</sub>, (c) HfO<sub>2</sub>, and (d) TiO<sub>2</sub> layer fractions for  $T_G=550^\circ\text{C}$  on Si for  $E=0$  kV/cm.
- Figure 3:** (Color online) Critical layer fraction of FE/DE bilayers as a function of the relative dielectric permittivity of the DE layer ( $T_G=550^\circ\text{C}$ ,  $E=0$  kV/cm) for Ti-rich PZT compositions.

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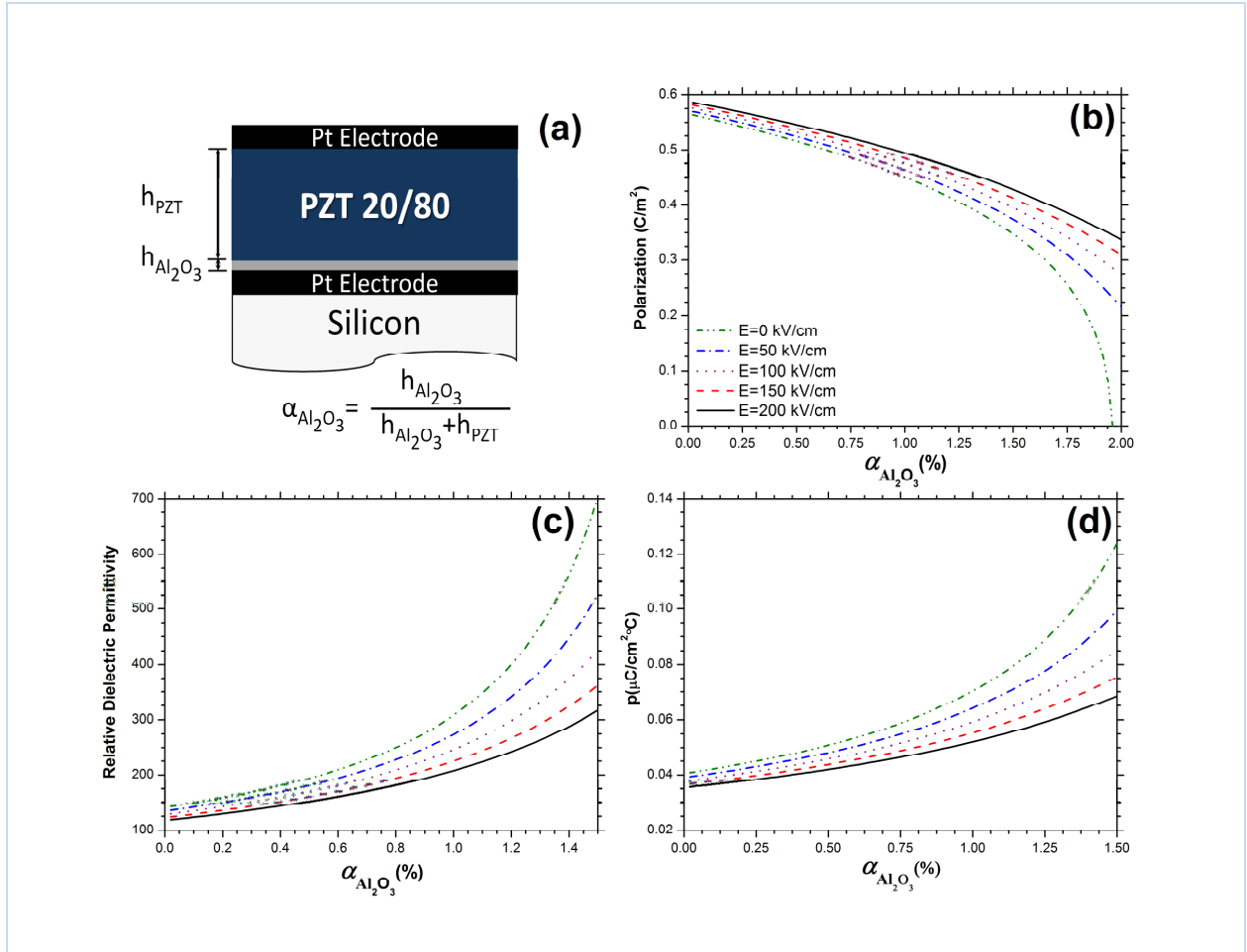


Figure 1

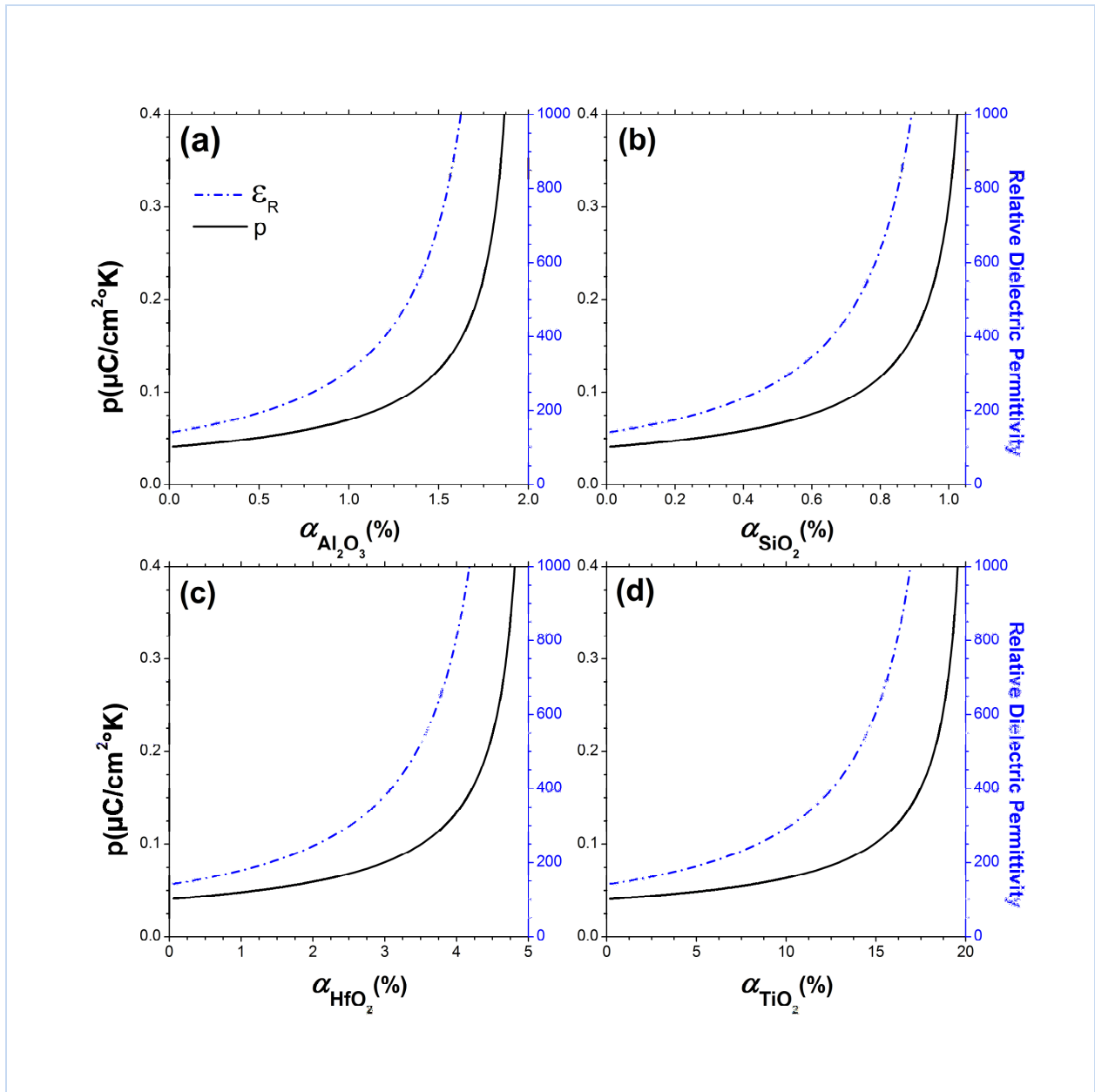


Figure 2

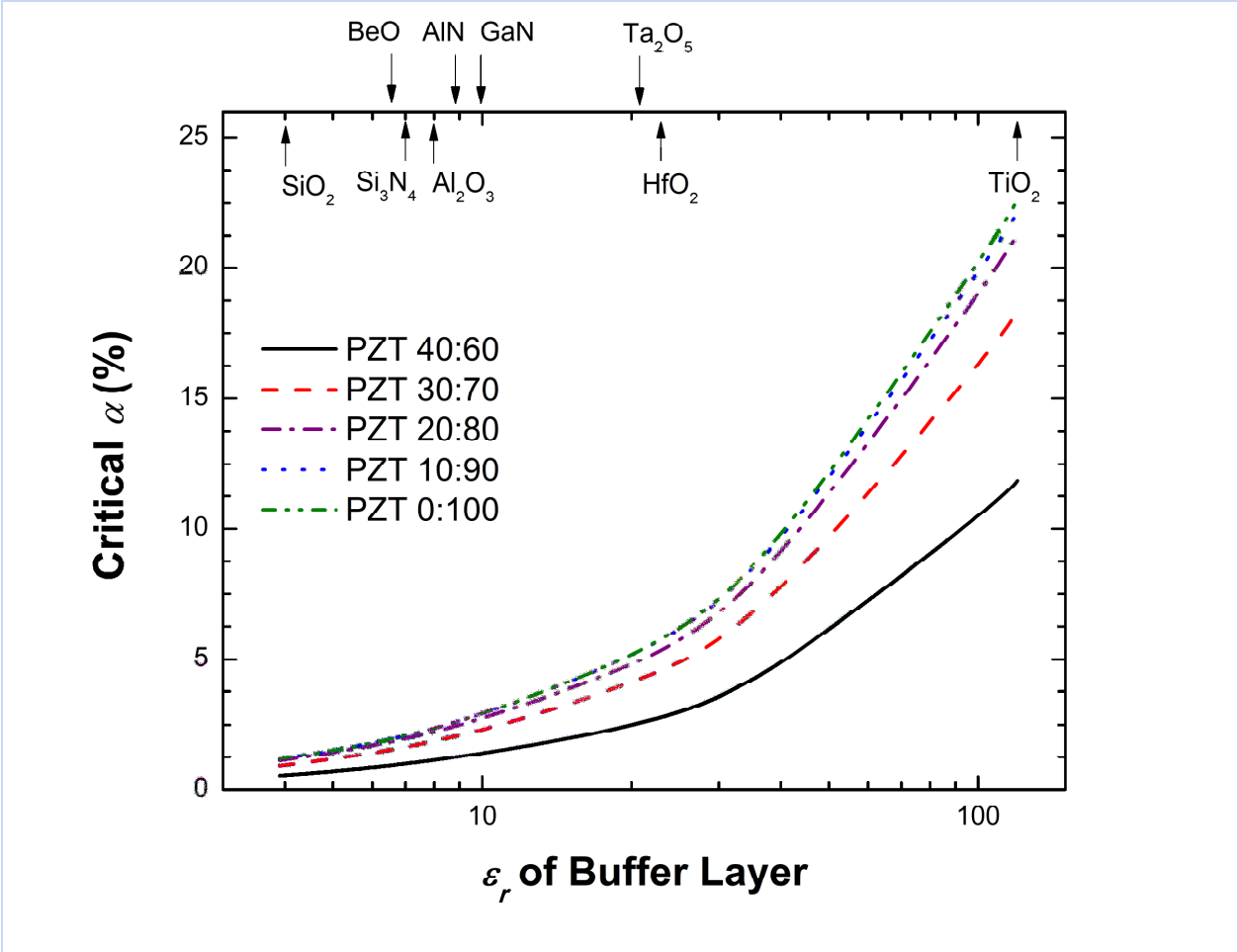


Figure 3